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Field proving of a liquid displacement meter using Bidirectional Pipe Provers in Custody Transfer applications; case study of Libyan Zueitina Oil Port

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ARTICLE INFOR

ABSTRACT

	In this paper, a field study is conducted on proving a posi-							
Article history:	displacement meter with bi-directional pipe provers to determin							
Received 24/08/2024	the repeatability of the meter's generated pulses and the deviation							
Revised 08/10/2024	of the Meter Factor percentage during the Meter Proving process							
1000000001012021	at Zueitina Oil Port in Libya. Equipment, procedures,							
Accepted 13/102024	requirements, national and international standards, and							
Available online	precautions that will ensure accurate metering of fluids were							
31/10/2024	considered. Detailed calculations were achieved, as can be seen in							
	the given results average of total number of pluses (round trip),							
	Repeatability, corrected prover volume(CPV), corrected meter							
	volume (CMV), the new meter factor and deviation of meter							
	factor are 119,873.000 Pluses,0.01502 %,122.44614 Barrel (BBL),							
	122.405389 Barrel(BBL), 1.000333, and 0.1058%, respectively. The							
	findings of this research are consistent with national and							
	international standards.							

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Keywords: Custody Transfer applications, Bi-Directional Pipe Provers, Meter-proving process.

1. Introduction

In hydrocarbon logistics, custody transfer requires exact volume measurements, which must be subject to legal meteorological requirements and state meteorological

control [1]. Measurements of refined petroleum products (gasoline, diesel, and kerosene) have traditionally been performed using turbines [2], [3], and volumetric meters [4], [5]. The latter, specifically, are the meters of the highest metrological quality [6], [7]. It is a common misconception that measurement is an exact science. In reality, all measurements are simply estimates of the actual value measured, and the actual value can never be known. An estimate that implies that there is some degree of doubt about the accuracy of that measurement. Measurement uncertainty provides an indication of the quality or reliability of a measurement result [8].

Documenting the uncertainty in flows measured by fiscal flow gauge stations is essential in assessing the condition of these gauge stations. The authorities have requirements with respect to maximum uncertainty in order to guarantee national interests. Partners selling oil have an interest in uncertainty to secure their incomes. Ultimately, oil buyers have an interest in ensuring that they will not receive less oil than they pay for. To get all parties to agree to an uncertainty analysis, it is important to obtain standardized ways to perform such an analysis. In 1995, the International Organization for Standardization (ISO) published the "Guide to the expression of uncertainty in measurement" [9].

Moreover, proving methods that utilize incremental uncertainty analysis to determine when proving is finished will give operators the chance to achieve even greater efficiency. To confirm this method, it is necessary to keep collecting runs until the repeatability is equivalent to a meter factor random uncertainty of better than 0.027%. API MPMS Ch. 4.8 prescribes several different methods that can be applied to assess the repeatability of proving data. The objective of their design is to ensure that the average meter factor result is not above 0.027%. In case repeatability fails, it is typical to discard the data and begin a new proving attempt .To determine the uncertainty of the meter factor, it is important to determine the repeatability of the meter factor average or pulses generated during proving. This study calculated the most important parameters, including the repeatability of pulses generated by the meters and the deviation of the Meter Factor percentage during the Meter Proving process at Zueitina Oil Port in Libya.

A map illustrated in Figure 1 shows the location of Zueitina Oil Port in Libya. Zueitina Oil Port is located in Libya near the town of Ajdabiya on the coast of the Mediterranean Sea. Also, it is situated in the East of Benghazi. It is owned by the Libyan National Corporation (NOC). The company's production is from its field in the south of Ajdabiya city. Zueitina Oil port is responsible for all types of oil that arrive at the port from reaching the export stage. It receives three types of crude oil, in addition to condensed naphtha, and the types of crude oil that are received are Zueitina crude, Abu At-Tafel crude, and pure Zueitina crude. These types of crude oil and condensed naphtha are also stored and shipped through it. All operations are monitored and controlled, including receiving, storing, and shipping crude oil and condensed naphtha.



Figure 1. Map of Zueitina Oil Port (LIBYA)

2. Methodolgy

There are methods of proving a meter: proving a meter with a pipe prover, proving a meter with an open tank prover, and proving a meter with a master meter.

For this research, proving of a positive displacement meter (meter number 205) with a pipe prover in" Zueitina Oil Port– Libya "will be carried out as a case study for the export of Zueitina crude according to the procedures and requirements mentioned in National and International standards.

Positive Displacement flow meter with bi-directional prover

Positive Displacement flow meter (number 205) selected in this study is shown in Figure 2.

Field proving of a liquid displacement meter using Bi-directional Pipe ...



Figure2. Positive Displacement flow meter

Bi-directional prover selected in this study is shown in Figure 3.



Figure 3. Bi-directional prover

Preparation of proving report

A Positive Displacement Meter-proving using Bi Directional Prover is illustrated in Figure 4



Figure 4. Bi Directional Prover

A sample proving report illustrated in Table 1 will be applicable to reflect the correlations and information. During the preparation of this paper, Meter-proving requirements and procedures, troubleshooting, and Converting volumes to standards maintained in the American Petroleum Institute (API) and Libyan Measurement standards [10-18] should be taken into consideration at Zueitina Oil port.

Calculations of sections of the proving report will be presented according to the American Petroleum Institute (API) [10] as follows:

Repeatability % = [(Highest Run – Lowest Run)/Lowest Run] × 100.....(1)

• To determine the corrected prover volume, multiplying the observed prover volume with all certain correction factors to convert the volume to standard temperature and Pressure as shown in Eq(2).

Corrected prover volume(CPV) = $BPV \times Ctsp \times Cpsp \times Ctlp \times Cplp$(2)

• To determine the corrected meter volume(*CMV*), *Average*d pulse count is divided by *number of Pulses* per barrel (k-factor), then multiplying with all certain correction factors to convert the volume to standard temperature and Pressure as shown in Eq(3).

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(CMV) = (Average Number of Pulses ÷ KF) * Ctlm * Cplm.....(3)
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- Once both volumes have been corrected to standard temperature and pressure , the meter factor is determined by dividing the corrected prover volume (CPV) by the corrected meter volume (CMV) as shown in Eq(4)
 (*MF*)= (*CPV*) ÷ (CMV)(4)
- Deviation of Meter Factor : Deviation of Meter Factor is calculated according to Eq(5)

Deviation (%) = [(New M Factor - Previous M Factor) / Previous M Factor]*100 ... (5)

3. Results

For guidance in interpreting the data on this report, calculations of sections of the report were explained in Table 1 as follows:

Field proving of a liquid displacement meter using Bi-directional Pipe ...

Date of Proving:	01/07/2	023 C	ompany	Zueitina Oil	Port	Location	Zueitina cit	y-libya
	Meter					Prover		
No	Serial No	Model	Size "İnches"	K facto: PULSES/E	r 3BL	BASE VOLUME AT 60°F AND "0" PSI (BPV)	OD SIZE "inches"	WT WALL "İnches"
205	45778888	PD	16 "	956.878	41	125.140020	26 "	0.375 "
 Liquid Data				Provious Roport				
Tuno	A PL et (0.0%E Eleve Dete			Elow Rate	o(hnh)	Provious	meter Factor	
7uoitin		0.01 11	low Rate		e(opii)	Tievious	meter ractor	
Crude	a 39.8 8000 bbl/hr			8000 bbl/hr		0.999052		
	Run Prove		over	Meter		METER COUNTER		_
	No	Temp (F)	Press(ps)	Temp(F)	Press psig	total nur for th	mber of pluses e round trip	
	1	106	54	105	53	í	119,877	
	2	106	54	105	53	-	119,860	
	3	106	54	105	53	-	119,878	
	4	106	54	105	53	-	119,877	
	5	106	54	105	53	-	119,877	
	AVG					11	9,873.000	
	Repeatability % 0		0.01502 %	502 % acceptable				_
	A	В	С	D		E F	F=A*B*C*D*E	
	BPV (BB	L) CTS _]	p CPS	p CTI	_p	CPLp	CPV (BBL)	
	125 1400	20 1 0008	200 1.000	1 0.07	72	1 0003	177 11611	

Table 1. Meter Prover Report

G	Η	I=G/H	J	К	L=I*J*K		
AVERGE PULES	K FACTOR	IV (BBL)	CTLm	CPLm	CMV(BBL)		
119,873.000	956.87841	125.2750597644	0.9768	0.9768	122.405389		
M=F/L N=H/M							
Me	ter Factor		NEW K FACTOR				
1	.000333		956.5598				

Deviation (%) = [(New M Factor – Previous M Factor) / Previous M Factor]

0.1058 %, "acceptable"

3. Discussion

As can be seen in the given results average of the total number of pluses (round trip), repeatability, corrected prover volume (CPV), corrected meter volume (CMV), the new meter factor and deviation of meter factor are 119,873.000 Pluses, 0.01502 %, 122.44614 Barrel (BBL), 122.405389 Barrel(BBL), 1.000333, and 0.1058%, respectively. This discussion will focus on understanding the most important parameters as follows:

- Repeatability % is equal to 0.01502 %, which is acceptable according to the American Petroleum Institute (API) and Libyan Measurement standards [12-15], which recommend that, proving runs must be made until the calculated meter factor or meter generated pulses from five consecutive runs match within a tolerance of 0.0005 (0.05 percent) between the highest and the lowest value.
- The deviation of Meter Factor % in this paper is equal to 0.1058% -, which is an acceptable one according to Libyan Measurement standards [12,13], which recommend that the new meter factors should be within +/- 0.003 (0.3%) of the previous meter factors. The deviation of Meter Factor % obtained from this study is also acceptable according to the American Petroleum Institute (API) [16], which states that common practice for custody transfer applications is to accept new meter factors under like operating conditions within (0.001) 0.10 % to (0.005) 0.50% of the previous meter factor.

4. Conclusions

A comprehensive and detailed operation, computations, requirements, and procedures of meter proving using conventional bi-directional pipe prover of Zueitina oil port– Libya has been presented. The findings of this research are consistent with national and international standards. However, the results obtained show that regular proving, checkups of meters; and following the procedures and requirements of meter proving according to the national and international standards, would improve metering and lead to success in implementing the Meter-proving process and ensure that measurements are accurate, allowing operations to proceed in a safe and timely manner

References

- [1] Lynnworth, L. C., & Liu, Y. (2006). Ultrasonic flowmeters: Half-century progress report, 1955–2005. Ultrasonics, 44, e1371-e1378.
- [2] Tawackolian, Karsten, Oliver Büker, Jankees Hogendoorn, and Thomas Lederer. "Calibration of an ultrasonic flow meter for hot water." Flow Measurement and Instrumentation 30 (2013): 166-173.
- [3] Anklin, M., Drahm, W., & Rieder, A. (2006). Coriolis mass flowmeters: Overview of the current state of the art and latest research. Flow Measurement and Instrumentation, 17(6), 317-323.
- [4] Wang, T., & Baker, R. (2014). Coriolis flowmeters: a review of developments over the past 20 years, and an assessment of the state of the art and likely future directions. Flow Measurement and Instrumentation, 40, 99-123.
- [5] Wang, T., & Hussain, Y. (2006). Investigation of the batch measurement errors for singlestraight tube Coriolis mass flowmeters. Flow measurement and Instrumentation, 17(6), 383-390.
- [6] Kalotay, P. (1999). Density and viscosity monitoring systems using Coriolis flow meters. ISA transactions, 38(4), 303-310.
- [7] Samer, G., & Fan, S. (2010). Modeling of Coriolis mass flow meter of a general plane-shape pipe. Flow Measurement and Instrumentation, 21(1), 40-47.
- [8] "Flow Measurement Uncertainty and Data Reconciliation" (2008), National measurement System (NEL).
- [9] JCGM 100:2008 GUM 1995 with minor corrections, Evaluation of measurement data Guide to the expression of uncertainty in measurement.
- [10] API MPMS 4.1: "Manual of Petroleum Measurement Standards Chapter 4: Proving Systems, Section 1 - Introduction," American Petroleum Institute, Washington DC, 2005;
- [11] API Manual of Petroleum Measurement Standards Chapter 4.8 Operation of Proving Systems Second Edition", American Petroleum Institute, Washington DC, 2013;

- [12] libyan Hydrocarbon's National Code for Dynamic &Static Measurement Systems Custody, Fiscal, Allocation, and Production Measurements Applications - National Oil Corporation (NOC) – Libya- General Department of Inspection & Measurement, October 2020;
- [13] ISO 9001:2015 Standard- quality management system NOC Inspection & Measurement General Directorate- LIBYA, December 2023;
- [14] API MPMS 12.2: "Manua' of Petroleum Measurement Standards Chapter 12: Calculation of Petroleum Quantities, Section 2 - Calculation of Petroleum Quantities Using Dynamic Measurement Methods and Volumetric Correction Factors, II Part 1-5, American Petroleum Institute, Washington DC, 1995 (Part 1),2003 (Part 2), 1998 (Part 3), 1997 (Part 4), 2001 (Part 5);
- [15] API MPMS 4.2: "Manual of Petroleum Measurement Standards Chapter ProvingSystems, Section 2 - Displacement Provers," American PetroleumInstitute, Washington DC, 2003;
- [16] "Manual of Petroleum Measurement Standards Chapter 5: Metering, Section 8 -Measurement of Liquid Hydrocarbons using UltrasonicFlow Meters," American Petroleum Institute, Washington DC, 2011;
- [17] Manual of Petroleum Measurement Standards Chapter 11: Physical Properties Data, Section 1 - Temperature and Pressure Volume Correction Factors (VCF) Software for Generalized Crude Oils,' Refined Products, and Lubricating Oils," American Petroleum Institute, Washington DC, 2004;
- [18] "Manua' of Petroleum Measurement Standards Chapter 12: Calculation of Petroleum Quantities, Section 2 - Calculation of Petroleum Quantities Using Dynamic Measurement Methods and Volumetric Correction Factors, II Part 1-5, American Petroleum Institute, Washington DC, 1995 (Part 1),2003 (Part 2), 1998 (Part 3), 1997 (Part 4), 2001 (Part 5);